Numerical Simulations of Evaporation and Condensation of Water in a Thermoacoustic Engine

熱音響エンジンにおける水の蒸発、凝縮の数値シミュレーショ ン

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1. Introduction

It has been experimentally reported that the critical temperature difference for sound generation in a thermoacoustic engine with a wet stack is considerably smaller than that with a dry stack¹. Raspet and his coworkers²⁻⁴ have studied the effect evaporation and condensation of on а thermaocoustic engine based on the Eulerian point of view. The aim of the present study is to understand dynamical effect of evaporation and condensation based on the Lagrangian point of view⁵.

There have already been some theoretical models of a thermoacoustic engine based on the Lagrangian point of view^{6, 7}. The model of the present paper is unique because Rott equations are taken into account for the first time in such models based on the Lagrangian point of view.

2. Model

Translational motion as well as expansion and contraction of a fluid parcel is numerically simulated (Fig. 1)⁵. The amplitudes of acoustic pressure and particle velocity are calculated as a function of position along a narrow tube using Rott equations. The instantaneous acoustic pressure and particle velocity are calculated at a position of a fluid parcle using their amplitudes at the position. Using instantaneous particle velocity, traslational motion of a fluid parcel is simply calculated as follows.

$$x(t + \Delta t) = x(t) + u\Delta t \tag{1}$$

where x(t) is a position of a fluid parcle at time t, Δt is a small time step, and u is instantaneous particle velocity at time t and position x.

While number of air molecules is constant in a fluid parcel, number of water vapor molecules changes with time by evaporation and condensation⁵. The instantaneous volume of a fluid parcel is determined by instantaneous pressure, temperature, and number of molecules inisde a fluid parcel as follows.



Fig. 1 A fluid parcel in a narrow tube in a stack of a thermoacoustic engine. Reprinted with permission from K.Yasui and N.Izu: J.Acoust.Soc.Am. **141** (2017) 4398. Copyright (2017), Acoustical Society of America.

 $V(t) = n_t(t)R_GT(t)/p(t)$ (2) where V(t) is instantaneous volume of a fluid parcel, $n_t(t)$ is instantaneous number of molecules of air and water vapor inisde a fluid parcel in mol, R_G is the universal gas constant, T(t) is instantaneous temperature of a fluid parcel, and p(t) is instantaneous pressure inisde a fluid parcel.

3. Results and Discussions

The results of numerical simulations for a traveling-wave thermoacoustic engine are shown in Fig. 2 (a) and (b) for a dry and a wet stack, respectively⁵. Volume oscillation amplitude of a fluid parcel is increased by evaporation and condensation because evaporation (condensation) takes place at the expansion (contraction) of a fluid parcel. Accordingly, pV work done by a fluid parcel increases by evaporation and condensation. It implies that sound intensity increases by evaporation and condensation.

Another finding is the gradual shift of the mean position of a fluid parcel to higher temperature side, which is acoustic streaming. It

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originates in Rott equations. However, detailed mechanism is very complicated, and will be studied in future in another paper.

On the other hand, volume oscillation amplitude decreases by evaporation and condensation for a standing-wave thermoacoustic engine⁵. Nevertheless, slight presence of traveling-wave component results in the increase in pV work by evaporation and condensation. For the definition of traveling-wave component, see Ref. 8.



(a)



(b)

Fig. 2 The result of the numerical simulations for a traveling-wave thermoacoustic engine on x-V diagram of a fluid parcel. (a) For a dry stack. (b) For a wet stack. Reprinted with permission from K.Yasui and N.Izu: J.Acoust.Soc.Am. **141** (2017) 4398. Copyright (2017), Acoustical Society of America.

4. Conclusion

Under many conditions, volume oscillation amplitude of a fluid parcel is increased by evaporation and condensation in a wet stack of a thermoacoustic engine. Accordingly, pV work done by a fluid parcel increases by evaporation and condensation. It implies that sound intensity increases by the effect. The present model based on the Lagrangian point of view is nonlinear and results in acoustic streaming. The acoustic streaming originates in Rott equations. However, difference and similarity of the acoustic streaming to Gedeon and Rayleigh streaming are unclear at present⁹⁻¹³, and will be studied in future.

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References

- 1. K.Tsuda and Y.Ueda: AIP Adv. 5 (2015) 097173.
- 2. R.Raspet, C.J.Hickey, and J.M.Sabatier: J. Acoust. Soc. Am. **105** (1999) 65.
- R.Raspet, W.V.Slaton, C.J.Hickey, and R.A.Hiller: J. Acoust. Soc. Am. 112 (2002) 1414.
- 4. W.V.Slaton, R.Raspet, C.J.Hickey, and R.A.Hiller: J. Acoust. Soc. Am. **112** (2002) 1423.
- 5. K.Yasui and N.Izu: J. Acoust. Soc. Am. 141 (2017) 4398.
- 6. R.S.Wakeland and R.M.Keolian: J. Acoust. Soc. Am. **116** (2004) 294.
- 7. K.I.Matveev, G.W.Swift, and S.Backhaus: Intern. J. Heat Mass Transfer **49** (2006) 868.
- 8. K.Yasui, T.Kozuka, M.Yasuoka, and K.Kato: J. Korean Phys. Soc. 67 (2015) 1755.
- 9. G.W.Swift, *Thermoacoustics: A Unifying Perspective for Some Engines and Refrigerators* (Acoustical Society of America, New York, 2002).
- 10. N.Sugimoto: J. Fluid Mech. 797 (2016) 765.
- 11. D.Gedeon, *Cryocoolers 9*, edited by R.G.Ross (Plenum, New York, 1997), p. 385.
- M.Mironov, V.Gusev, Y.Auregan, P.Lotton, M.Bruneau, and P.Piatakov, J.Acoust.Soc.Am. 112 (2002) 441.
- 13. V.Gusev, S.Job, H.Bailliet, P.Lotton, and M.Bruneau, J.Acoust.Soc.Am. 108 (2000) 934.